## American Institute of Timber Construction

## Design Table for Pitched and Curved Beams

This design table contains the widths, depths, radii, and reinforcing requirements of pitched and curved beams of constant cross section with mechanically attached haunches for commonly used roof slopes, spans, and loading.

| Design Load <br> Roof dead load plus roof live load | Roof Slope | 40 Ft Span |  | 50 Ft Span |  | 60 Ft Span |  | 80 Ft Span |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | SIZE | R | SIZE | R | SIZE | R | SIZE | R |
|  |  | Lag Screws | Rebar | Lag Screws | Rebar | Lag Screws | Rebar | Lag Screws | Rebar |
| 400 plf | 2/12 | None Required |  | None Required |  | $6-3 / 4 \times 33$ <br> None Re | $\begin{aligned} & \text { 91'- 6" } \\ & \text { גired } \end{aligned}$ | $\begin{array}{r} 8-3 / 4 \times 43-1 / 2 \\ \text { None Rec } \end{array}$ | $\text { 121'- } 11 \text { " }$ <br> uired |
|  | 3/12 | $\begin{gathered} \hline 5-1 / 8 \times 22-1 / 2 \\ 22-3 / 4 \mathrm{in} . \\ \hline \end{gathered}$ | $\begin{gathered} 41 \text { '-3" } \\ 22-- \text { \#3 } \end{gathered}$ | $\begin{gathered} 5-1 / 8 \times 28-1 / 2 \\ 22--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} 51 '-6 " \\ 22--\# 3 \end{gathered}$ | $6-3 / 4 \times 34-1 / 2$ <br> None Regu | $\begin{aligned} & \text { 61'-9" } \\ & \text { uired } \end{aligned}$ | $8-3 / 4 \times 43-1 / 2 \quad 82^{\prime}-4 "$None Required |  |
|  | 4/12 | $\begin{gathered} \hline 5-1 / 8 \times 22-1 / 2 \\ 22-3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{aligned} & \text { *32'- 0" } \\ & 22 \text {-- \#3 } \end{aligned}$ | $\begin{gathered} \hline 5-1 / 8 \times 28-1 / 2 \\ 22--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} \hline 39 '-6 " \\ 22--\# 3 \end{gathered}$ | $\begin{gathered} 6-3 / 4 \times 33 \\ 22--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} \hline 47 '-6 " \\ 22-\text { \#3 } \end{gathered}$ | $\begin{gathered} \hline 8-3 / 4 \times 43-1 / 2 \\ 23--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} 63 '-3 " \\ 23-\text { - \#3 } \end{gathered}$ |
|  | 5/12 | $\begin{gathered} \hline 5-1 / 8 \times 22-1 / 2 \\ 22-3 / 4 \mathrm{in} . \\ \hline \end{gathered}$ | $\begin{aligned} & \text { *32'- 0" } \\ & 22 \text {-- \#3 } \end{aligned}$ | $\begin{gathered} \hline 5-1 / 8 \times 28-1 / 2 \\ 22--3 / 4 \mathrm{in.} \\ \hline \end{gathered}$ | $\begin{gathered} \hline 32 '-6 " \\ 22--\# 3 \\ \hline \end{gathered}$ | $\begin{array}{r} 6-3 / 4 \times 33 \\ 22--7 / 8 \mathrm{in} . \\ \hline \end{array}$ | $\begin{gathered} 39 '-0 " \\ 22--\# 3 \\ \hline \end{gathered}$ |  |  |
|  | 2/12 | None Required |  | None Required |  | $\begin{array}{r} \hline 6-3 / 4 \times 37-1 / 2 \\ \text { None Re } \end{array}$ | $\begin{aligned} & \text { 91'- 6" } \\ & \text { uired } \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline 8-3 / 4 \times 49-1 / 2 \\ \text { None Rec } \\ \hline \end{array}$ | $\begin{aligned} & 121^{\prime}-11^{\prime \prime} \\ & \text { uired } \end{aligned}$ |
|  | 3/12 | $\begin{gathered} 5-1 / 8 \times 27 \\ 18--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} 41^{\prime}-3^{\prime \prime} \\ 18-- \text { \#3 } \end{gathered}$ | $\begin{gathered} 6-3 / 4 \times 30 \\ 20--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} 51 '-6 " \\ 20--\# 3 \end{gathered}$ | $\begin{gathered} 6-3 / 4 \times 37-1 / 2 \\ 20--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} 61^{\prime}-9 " \\ 20-- \text { \#3 } \end{gathered}$ | $\begin{gathered} \hline 8-3 / 4 \times 49-1 / 2 \\ 20--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} 82 '-4 " \\ 20-\text { - \#4 } \end{gathered}$ |
|  | 4/12 | $\begin{gathered} 5-1 / 8 \times 27 \\ 18--3 / 4 \mathrm{in} . \\ \hline \end{gathered}$ | $\begin{aligned} & \text { *32'- 0" } \\ & 18-- \text { \#3 } \end{aligned}$ | $\begin{gathered} 6-3 / 4 \times 30 \\ 20--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} \hline 39^{\prime}-6 \text { " } \\ 20--\# 3 \\ \hline \end{gathered}$ | $\begin{gathered} 6-3 / 4 \times 37-1 / 2 \\ 20--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} \hline 47 '-6 " \\ 20--\# 4 \end{gathered}$ | $\begin{gathered} \hline 8-3 / 4 \times 49-1 / 2 \\ 20--7 / 8 \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} 63 '-3^{\prime \prime} \\ 20--\# 4 \end{gathered}$ |
|  | 5/12 | $\begin{array}{\|c\|} \hline 5-1 / 8 \times 28-1 / 2 \\ 17-3 / 4 \mathrm{in} . \end{array}$ | $\begin{aligned} & \text { *32'- 0" } \\ & 17-- \text { \#3 } \end{aligned}$ | $\begin{gathered} \hline 6-3 / 4 \times 31-1 / 2 \\ 20--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} \hline 32 '-6 " \\ 20--\# 4 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 6-3 / 4 \times 37-1 / 2 \\ 20--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} 39 '-0 " \\ 20--\# 4 \\ \hline \end{gathered}$ |  |  |
|  | 2/12 | $\begin{array}{\|c\|} \hline 5-1 / 8 \times 31-1 / 2 \\ 16--3 / 4 \text { in. } \\ \hline \end{array}$ | $\begin{gathered} 61 '-0 " \\ 16-- \text { \#3 } \\ \hline \end{gathered}$ | $\begin{gathered} 6-3 / 4 \times 36 \\ 17--3 / 4 \mathrm{in} . \\ \hline \end{gathered}$ | $\begin{gathered} \hline 76^{\prime}-3^{\prime \prime} \\ 17--\# 3 \\ \hline \end{gathered}$ | $\begin{gathered} 6-3 / 4 \times 43-1 / 2 \\ 17--3 / 4 \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \hline 91 '-6 " \\ 17--\# 3 \\ \hline \end{gathered}$ | $\begin{array}{cc} \hline 8-3 / 4 \times 54 \quad 121^{\prime}-11^{\prime \prime} \\ \text { None Required } \end{array}$ |  |
|  | 3/12 | $\begin{gathered} \hline 5-1 / 8 \times 31-1 / 2 \\ 16--3 / 4 \mathrm{in} . \\ \hline \end{gathered}$ | $\begin{gathered} 41^{\prime}-3^{\prime \prime} \\ 16-- \text { \#3 } \end{gathered}$ | $\begin{gathered} 6-3 / 4 \times 36 \\ 17--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} 51 '-6 " \\ 17--\# 3 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 6-3 / 4 \times 43-1 / 2 \\ 17--3 / 4 \mathrm{in.} \end{gathered}$ | $\begin{gathered} 61^{\prime}-9 " \\ 17--\# 4 \\ \hline \end{gathered}$ | $\begin{gathered} 8-3 / 4 \times 54 \\ 20--3 / 4 \mathrm{in.} \end{gathered}$ | $\begin{gathered} 82^{\prime}-4^{\prime \prime} \\ 20-- \text { \#4 } \end{gathered}$ |
|  | 4/12 | $\begin{array}{\|c\|} \hline 5-1 / 8 \times 31-1 / 2 \\ 16--3 / 4 \mathrm{in} . \end{array}$ | $\begin{aligned} & \text { *32'- 0" } \\ & 16-- \text { \#3 } \end{aligned}$ | $\begin{gathered} 6-3 / 4 \times 36 \\ 17--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} \hline 39^{\prime}-6 "^{\prime \prime} \\ 17--\# 4 \end{gathered}$ | $\begin{gathered} \hline 6-3 / 4 \times 43-1 / 2 \\ 17 \text {-- } 7 / 8 \mathrm{in.} \end{gathered}$ | $\begin{gathered} \hline 47 '-6 " \\ 17--\# 4 \end{gathered}$ | $\begin{gathered} \hline 8-3 / 4 \times 54 \\ 20--7 / 8 \mathrm{in.} \end{gathered}$ | $\begin{gathered} 63 '-3 " \\ 20--\# 4 \end{gathered}$ |
|  | 5/12 | $\begin{gathered} 5-1 / 8 \times 33 \\ 15--3 / 4 \mathrm{in} . \\ \hline \end{gathered}$ | $\begin{aligned} & \text { *32'- 0" } \\ & 15-- \text { \#4 } \end{aligned}$ | $\begin{gathered} 6-3 / 4 \times 36 \\ 17--7 / 8 \mathrm{in} . \end{gathered}$ | $\begin{gathered} \hline 32 '-6 " \\ 17--\# 4 \end{gathered}$ | $\begin{gathered} \hline 6-3 / 4 \times 43-1 / 2 \\ 17--7 / 8 \mathrm{in.} \end{gathered}$ | $\begin{gathered} 39 '-0 " \\ 17--\# 4 \end{gathered}$ |  |  |
|  | 2/12 | $\begin{gathered} 6-3 / 4 \times 30 \\ 16--3 / 4 \mathrm{in} . \\ \hline \end{gathered}$ | $\begin{gathered} 61 '-0 " \\ 16-- \text { \#3 } \end{gathered}$ | $\begin{gathered} 6-3 / 4 \times 39 \\ 16--3 / 4 \mathrm{in} . \\ \hline \end{gathered}$ | $\begin{gathered} 76 '-3^{\prime \prime} \\ 16-\text { \#3 } \end{gathered}$ | $8-3 / 4 \times 45$ None Re | $\begin{aligned} & \text { 91'- 6" } \\ & \text { uired } \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 8-3 / 4 \times 58-1 / 2 \\ 20--3 / 4 \mathrm{in} . \\ \hline \end{gathered}$ | $\begin{gathered} 121^{\prime}-11^{\prime \prime} \\ 20-- \text { } \\ \hline \end{gathered}$ |
|  | 3/12 | $\begin{array}{\|c\|} \hline 6-3 / 4 \times 31-1 / 2 \\ 16--3 / 4 \mathrm{in} . \end{array}$ | $\begin{gathered} 41^{\prime}-3^{\prime \prime} \\ 16-- \text { \#3 } \end{gathered}$ | $\begin{gathered} 6-3 / 4 \times 39 \\ 16--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{gathered} 51 '-6 " \\ 16--\# 4 \end{gathered}$ | $\begin{gathered} 8-3 / 4 \times 42 \\ 18--7 / 8 \mathrm{in} . \end{gathered}$ | $\begin{gathered} 61^{\prime}-9 " \\ 18--\# 4 \end{gathered}$ | $\begin{gathered} \hline 8-3 / 4 \times 58-1 / 2 \\ 20--7 / 8 \mathrm{in} . \end{gathered}$ | $\begin{gathered} 82 '-4 " \\ 20--\# 4 \end{gathered}$ |
|  | 4/12 | $\begin{gathered} \hline 6-3 / 4 \times 31-1 / 2 \\ 16--3 / 4 \mathrm{in} . \end{gathered}$ | $\begin{aligned} & \text { *32'- 0" } \\ & 16--~ \# 4 \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 6-3 / 4 \times 40-1 / 2 \\ 15--7 / 8 \mathrm{in.} . \\ \hline \end{gathered}$ | $\begin{gathered} 39 '-6 " \\ 15--\# 4 \end{gathered}$ | $\begin{gathered} \hline 8-3 / 4 \times 43-1 / 2 \\ 17--7 / 8 \mathrm{in} . \\ \hline \end{gathered}$ | $\begin{gathered} \hline 47 '-6 " \\ 17--\# 4 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8-3 / 4 \times 58-1 / 2 \\ 20--1 \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} 63^{\prime}-3^{\prime \prime} \\ 20-- \text { \#5 } \\ \hline \end{gathered}$ |
|  | 5/12 | $\begin{array}{\|c} \hline 6-3 / 4 \times 31-1 / 2 \\ 16--7 / 8 \mathrm{in} . \\ \hline \end{array}$ | $\begin{aligned} & \text { *32'- 0" } \\ & 16--\# 4 \end{aligned}$ | $\begin{gathered} 6-3 / 4 \times 40-1 / 2 \\ 15--7 / 8 \mathrm{in} . \end{gathered}$ | $\begin{gathered} 32^{\prime}-6 " \\ 15-\text { - \#4 } \end{gathered}$ | $\begin{gathered} \hline 8-3 / 4 \times 43-1 / 2 \\ 17--1 \mathrm{in} . \\ \hline \end{gathered}$ | $\begin{gathered} \hline 39 '-0 " \\ 17--\# 5 \\ \hline \end{gathered}$ |  |  |

Table Specifications:

* Tangent points are greater than $1 / 4$ of span from centerline. Except as noted, the tangent points on the soffit face of the beam are located at the $1 / 4$ points. Beams with radial reinforcement should be manufactured from lumber which has a maximum moisture content of $12 \%$. Lag screws must be fully threaded. Rebar and epoxy must conform to AITC 404-92 (found in AITC 200 Inspection Manual).
Reinforcement shall be equally spaced in curved portions.
Deflection limit is $1 / 180$ of the span for total load. Total load includes the weight of the beam. Beams shall
be laterally supported with adequate bracing along the length at the top and at the bottom at the ends.
Designs are based on uniformly distributed loads using load duration factor for construction live loads, $C_{D}=1.25$.
Design values used for this table are: $\quad \mathrm{F}_{\mathrm{bx}}=\quad 2400 \mathrm{psi} \quad \mathrm{F}_{\mathrm{vx}}=\quad 165 \mathrm{psi}$

$$
\mathrm{F}_{\mathrm{rt}}=\quad 15 \mathrm{psi} \quad \mathrm{E}_{\mathrm{x}}=1,800,000 \mathrm{psi}
$$

$$
\mathrm{F}_{\mathrm{rt}}=\quad 55 \mathrm{psi}, \text { when radial reinforcement is provided }
$$

While these designs have been prepared in accordance with recognized engineering principles and are based on accurate technical data available, designs should not be used without competent professional examination and verification of the accuracy, suitability, and applicability by a licensed design professional.

AITC MAKES NO REPRESENTATION OR WARRANTY, EXPRESSED OR IMPLIED, THAT THE INFORMATION CONTAINED HEREIN IS SUITABLE FOR ANY GENERAL OR SPECIFIC USE OR IS FREE FROM INFRINGEMENT OF ANY PATENT OR COPYRIGHT. ANY USER OF THIS INFORMATION ASSUMES ALL RISK AND LIABILITY ARISING FROM SUCH USE.

